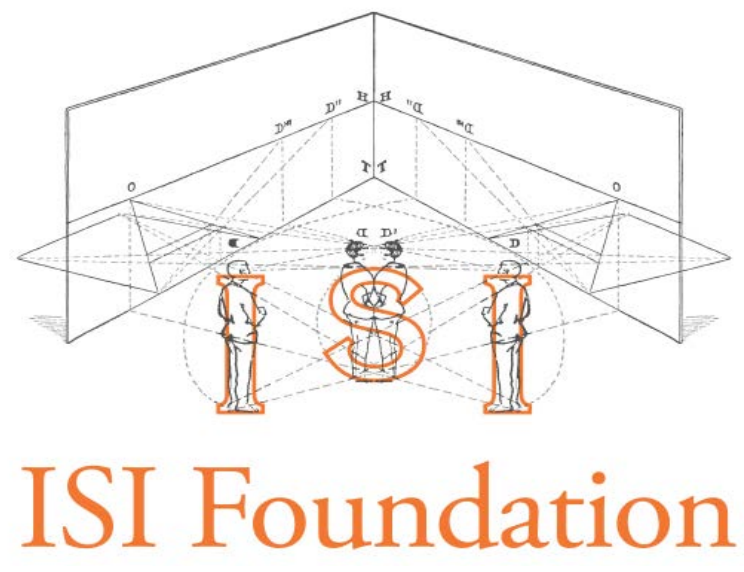


Analytical Modeling of Magnetic DW Motion



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1. Introduction

- Manipulating magnetic domain walls (DWs) within nanostructures has been linked with spintronic logic, storage and sensing devices.
- The 1-D model is the prime analytical model for describing magnetic DW motion [1-3]. While qualitatively successful, this model may at times fail to quantitatively match experimental and numerical results.

2. The Landau-Lifshitz Gilbert Equation

$$\frac{d\vec{m}}{dt} = -\gamma_0 \vec{m} \times \vec{H}_{eff} + \alpha \vec{m} \times \frac{d\vec{m}}{dt} + (\vec{u} \cdot \nabla) \vec{m} - \beta \vec{m} \times [(\vec{u} \cdot \nabla) \vec{m}] + \gamma_0 H_{FL} \vec{m} \times \hat{u}_{SOT} - \gamma_0 H_{SL} \vec{m} \times (\vec{m} \times \hat{u}_{SOT})$$

$$H_{eff} = -\frac{1}{\mu_0 M_s} \frac{\delta E}{\delta \vec{m}} \quad e_D = \frac{dE}{dV} = A \sum |\nabla \vec{m}_i|^2 + K_U \sin^2 \theta - \mu_0 M_s \vec{m} \cdot \vec{H}_a - \frac{1}{2} \mu_0 M_s \vec{m} \cdot \vec{H}_d + D [m_z \nabla \cdot \vec{m} - (\vec{m} \cdot \nabla) m_z]$$

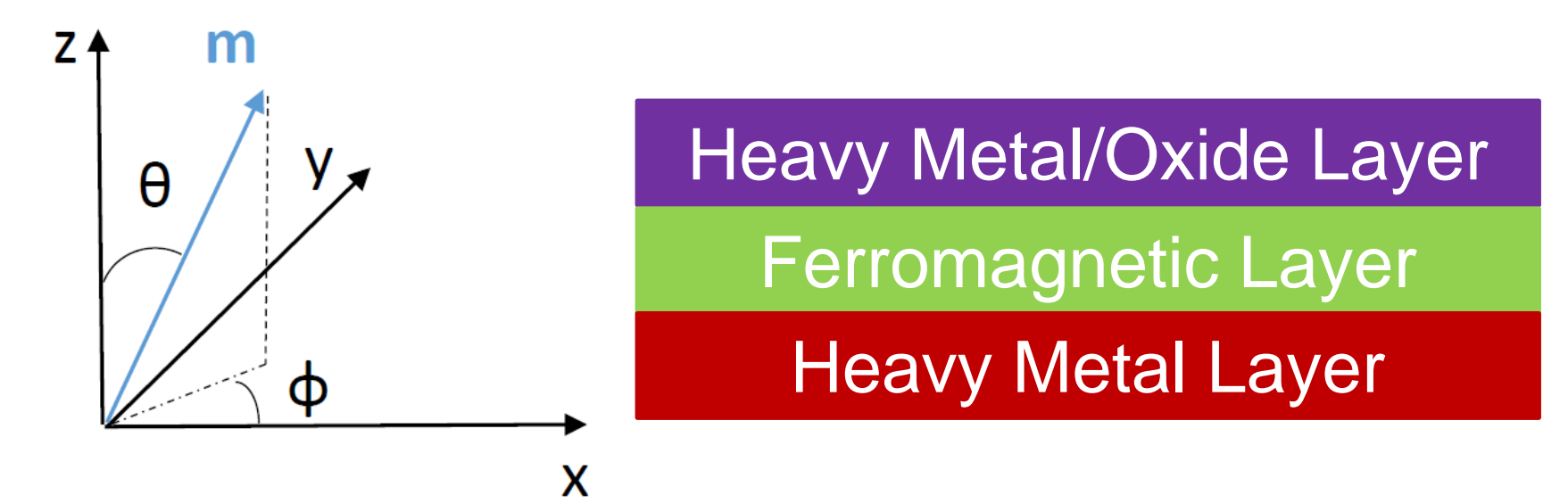


Fig. 1. Material and coordinate systems under study.

3. A Collective Coordinates Approach

Magnetic DWs in perpendicularly magnetized heterostructures may be described using a set of collective coordinates. We have selected the following 4 time-dependent coordinates which can lead to a generalized 1-D model:

- The position of the center of the DW (q)
- The tilt angle of the magnetization in the plane of the sample (ϕ)
- The domain wall width (Δ)
- The tilt angle of the wall (χ)

$$\phi(x, y, t) = \phi(t)$$

$$\theta(x, y, t) = 2 \operatorname{atan} \left(\exp \left(\frac{(x - q) \cos \chi + y \sin \chi}{\Delta} \right) \right)$$

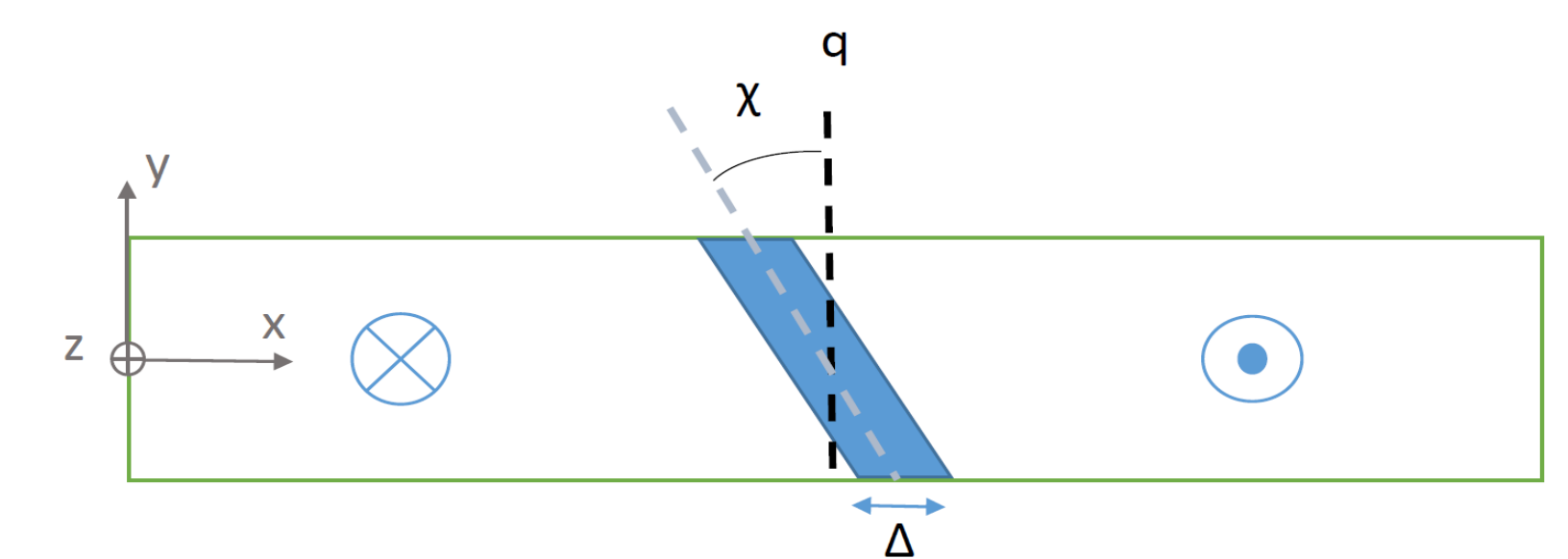


Fig. 2. Model of a tilted DW illustrating the collective coordinates.

$$(1 + \alpha^2) \frac{\dot{q}}{\Delta} \cos \chi = \alpha \mu_0 \gamma \left[H_z - \frac{\pi}{2} H_{sl} [\sin \phi u_{SOTx} - \cos \phi u_{SOTy}] \right] + (1 + \alpha \beta) \frac{u}{\Delta} \cos \chi + \mu_0 \gamma H_{sl} u_{SOTz} + \frac{1}{2} \gamma M_s (N_y - N_x) \sin 2(\phi - \chi) + \frac{\pi}{2} \left[\mu_0 \gamma [H_x \sin \phi - H_y \cos \phi] - \frac{\gamma D}{M_s \Delta} \sin(\phi - \chi) \right]$$

$$(1 + \alpha^2) \dot{\phi} = \mu_0 \gamma \left[H_z - \frac{\pi}{2} H_{sl} [\sin \phi u_{SOTx} - \cos \phi u_{SOTy}] \right] + (\beta - \alpha) \frac{u}{\Delta} \cos \chi - \alpha \mu_0 \gamma \tau_{sl} u_{SOTz} - \frac{\alpha}{2} \gamma M_s (N_y - N_x) \sin 2(\phi - \chi) - \alpha \frac{\pi}{2} \left[\mu_0 \gamma [H_x \sin \phi - H_y \cos \phi] - \frac{\gamma D}{M_s \Delta} \sin(\phi - \chi) \right]$$

$$\frac{\alpha}{2} \frac{1}{6} \left(\frac{w}{\Delta} \right)^2 \frac{\dot{\Delta}}{\Delta} = \frac{\gamma}{M_s} \frac{A}{\Delta^2} \left(\left(\frac{w}{\pi \Delta} \right)^2 + \sin^2 \chi \right) + \frac{\gamma}{M_s} \left(\frac{w}{\pi \Delta} \right)^2 \left[K_U + \frac{1}{2} \mu_0 M_s^2 (N_x \cos^2(\phi - \chi) + N_y \sin^2(\phi - \chi) - N_z) \right] - \frac{1}{2} \gamma c M_s (N_y - N_x) \cos \chi \sin 2(\phi - \chi) + \frac{\pi}{2} \frac{\gamma D}{M_s \Delta} \sin \phi + \frac{\pi}{2} \left(\frac{w}{\pi \Delta} \right)^2 \mu_0 \gamma [H_x \cos \phi + H_y \sin \phi]$$

$$-\frac{\alpha}{2} \frac{1}{6} \left(\frac{w}{\Delta} \right)^2 \frac{\dot{\chi}}{\cos \chi} = 2 \frac{\gamma}{M_s} \frac{A}{\Delta^2} \sin \chi - \frac{1}{2} \gamma M_s (N_y - N_x) \cos \chi \sin 2(\phi - \chi) + \frac{\pi}{2} \frac{\gamma D}{M_s \Delta} \sin \phi$$

4. Controlling DW Motion with In-plane Fields

In-plane fields could be used to control the direction of DW motion in PMA heterostructures, due to the Dzyloshinskii-Moriya Interaction (DMI).

$$(1 + \alpha^2) \frac{\dot{q}}{\Delta} \cos \chi = \frac{\pi}{2} H_{sl} \alpha \mu_0 \gamma \cos \phi + \frac{1}{2} \gamma M_s (N_y - N_x) \sin 2(\phi - \chi) + \frac{\pi}{2} \left[\mu_0 \gamma H_x \sin \phi - \frac{\gamma D}{M_s \Delta} \sin(\phi - \chi) \right]$$

$$H_{SL} = \frac{\hbar \theta_{SHE} J}{2 e M_s t_f}$$

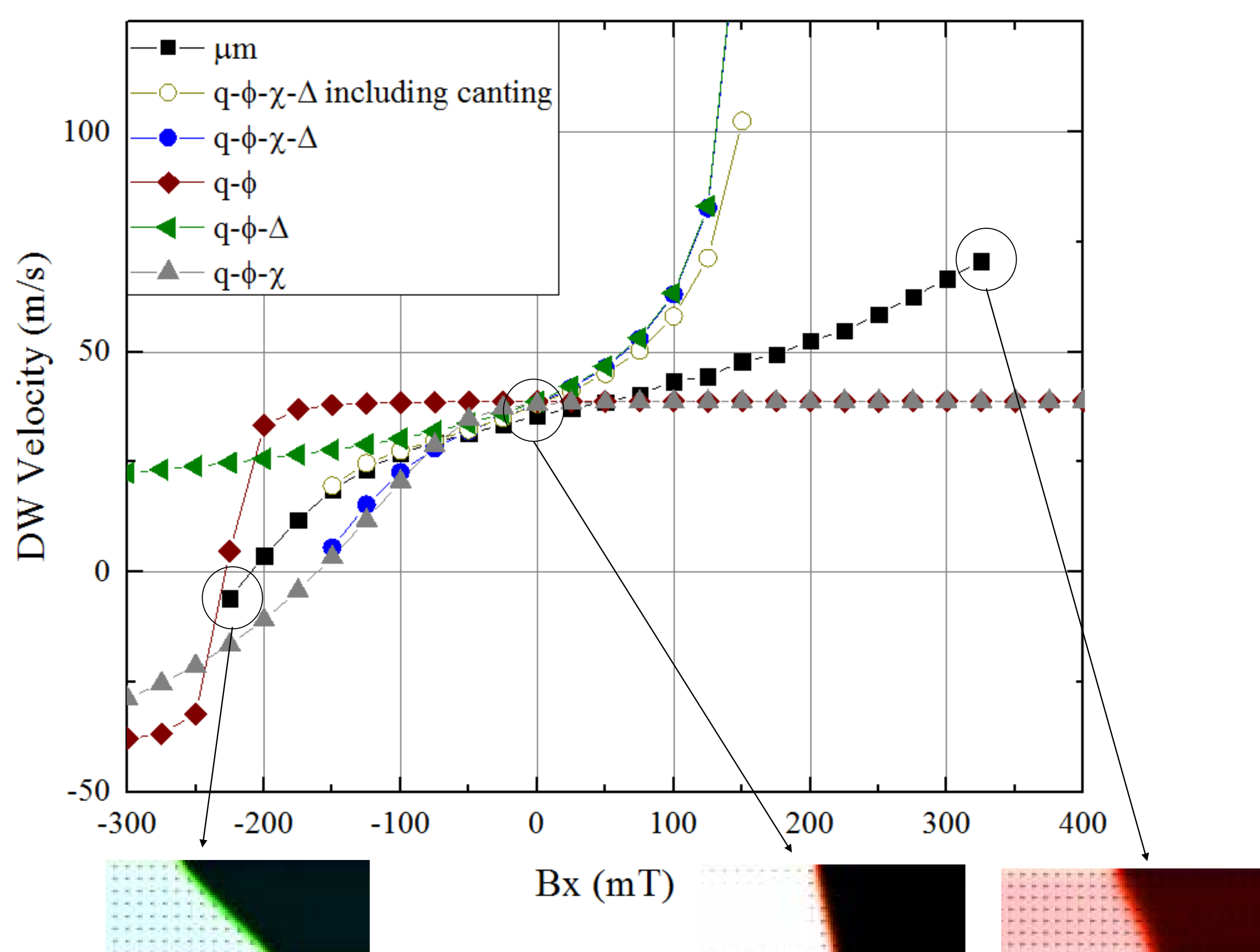


Fig. 2. SHE-driven DW motion under in-plane fields in a Pt-Co-Mgo heterostructure with high DMI. Material properties [4]: saturation magnetization $M_s = 700$ kA/m, exchange constant $A = 0.1$ pJ/m, uniaxial perpendicular anisotropy constant $K_U = 480$ kJ/m³, Gilbert damping $\alpha = 0.3$, SHE angle $\theta_{SHE} = 0.07$, Interfacial DMI $D = 1.2$ mJ/m².

5. Comparison to a Model based on Statistical Averages

- A model based on statistical averages has been proposed for field and spin-transfer torque driven DW motion [5].
- Provides a means of performing system identification (or as they call it "fingerprinting") on the system.
- Comparison to the analytical model could shed some light on the limitations and means of improving the analytical models.
- In a system with perpendicular magnetic anisotropy but no DMI:

$$1\text{-D Model} \quad (1 + \alpha^2) \dot{\phi} = \mu_0 \gamma H_z + (\beta - \alpha) \frac{u}{\Delta} - \alpha \gamma M_s (N_y - N_x) \frac{\sin 2\phi}{2}$$

$$\text{Ghent Model} \quad (1 + \alpha^2) \left(\delta \frac{\partial \Phi}{\partial t} \right) = \mu_0 \gamma H_z - (\beta - \alpha) \frac{u}{\left(\frac{L_x}{2} \right)} - \alpha \gamma M_s (N_y - N_x) \frac{\langle m_j \rangle \langle m_k \rangle}{\langle \delta \rangle}$$

$$\Phi = \operatorname{atan} \left(\frac{m_y}{m_x} \right) \quad \delta = m_j^2 + m_k^2$$

6. References

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